An electrospray technique for hyperquenched glass calorimetry studies: Propylene glycol and di-n-butyl phthalate

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Abstract

We describe an electrospray technique for in situ preparation, for differential scanning calorimetry study, of samples of molecular liquids quenched into the glassy state on extremely short time scales (hyperquenched). We study the cases of a hydrogen-bonded liquid, propylene glycol, PG and a Van der Waals liquid, di-n-butyl phthalate DBP. Using a fictive temperature method of obtaining the temperature dependence of enthalpy relaxation, we show that the electrospray method yields quenching rates of \(10^5\) K/s, while the more common method, dropping a sealed pan of sample into liquid nitrogen, yields only 120 K/s. These hyperquenched samples start to relax, exothermically, far below the glass temperature, at a temperature \((0.75T_g)\) where the thermal energy permits escape from the shallow traps in which the system becomes localized during hyperquenching. This permits estimation of the trap depths, which are then compared with the activation energy estimated from the fictive temperature of the glass and the relaxation time at the fictive temperature. The trap depth in molar energy units is compared with the ‘height of the landscape’ for PG, the quasi-lattice energy of the liquid based on the enthalpy of vaporization, and the single molecule activation energy for diffusion in crystals. The findings are consistent with the mechanism of relaxation invoked in a current model of relaxation in glassforming liquids. In the case of di-n-butyl phthalate we investigate the additional question of sub-\(T_g\) annealing effects. We find the ‘shadow’ glass transition, (an annealing prepeak) seen previously only in multicomponent mineral and metallic glasses. The phenomenon is important for understanding microheterogeneities in viscous liquid structures.

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1. Introduction

In recent studies we [1,2], and others [3,4], have stressed the importance of laboratory hyperquenching strategies in clarifying the physics of glassforming systems. Not only does vitrification on very short time scales help bridge the current gap between computer simulation investigations of supercooled liquids and their experimental counterparts, but it provides glassy materials in much higher states of configurational excitation than have previously been studied in appropriate detail. The properties of high fictive temperature glasses appear to differ in important ways from those of normal glasses (in particular they are much more structurally labile, and start relaxing as low as 2/3 of their normal \(T_g\)’s). Elucidating these differences will be important in refining our understanding of the structure and energetics of the viscous liquid state, and of the vitrification process itself.

The aging process in glasses, both of spin and structural types, has been the subject of many recent studies [5–8]. Those performed by molecular dynamics (computer modeling) methods [7,8] have been conducted on time scales of tens of ns, utilizing glasses formed on tenths of ns timescales and currently these can be extended to time...
scales in the microsecond domain [9]. By contrast, laboratory studies of aging have been largely conducted on glasses formed on the time scale of minutes, and aged on the time scale of days and weeks. By forming the glasses on very short time scales, however, the aging process can be observed at much lower temperatures [10,11] or, alternatively, on much shorter time scales at higher aging temperatures [12]. By studying the onset of relaxation of the hyperquenched glasses during reheating, the depth of the trap in which the glass was arrested (or the energy barrier to be overcome in structural relaxation) can be determined [2]. Then, by appropriate thermochemical methods (detailed below and elsewhere [1,3]), the temperature at which the system was arrested during the hyperquench can be obtained. Thus hyperquenching studies (which in the past have been used almost exclusively to vitrify systems that normally crystallize) can provide information on the energetics of the ‘liquid landscape’ [13,14] in energy ranges approaching those involved in computer simulation studies. In particular the hyperquenching studies provide access, or at least close approach, to the very interesting ‘crossover’ region that is currently much in focus for the case of fragile liquids [15–18]. This corresponds to the critical temperature $T_c$ of the mode coupling theory, the Stickel $T_b$ temperature (where temperature derivative analysis indicates a change in best fit Vogel-Fulcher-Tammann equation parameters, and frequently, but not always, the $\alpha$–$\beta$ relaxation bifurcation temperature [19]. Some [16,20], have recommended the use of $T_x$ to designate this crossover temperature.

Hyperquenching studies, like their computer simulation counterparts, depend for their usefulness on the very large gap in the time scales on which the distinct vibrational and configurational degrees of freedom of a viscous liquid are explored. This separability of degrees of freedom is manifested most directly in the familiar glass transition [15b,21] at which the configurational, but not the vibrational, contribution to the liquid heat capacity drops out. It drops out because its exploration time scale exceeds that of the heat capacity-determining experiment. In effect, the system becomes trapped in one of the innumerable minima on the potential energy hypersurface in configuration space [22–24] and thereafter acts like a crystal (single structure) system, in which only vibrational modes can be excited. This phenomenology concerning the $\alpha$-relaxation is all quite well understood, and hyperquenching studies will only confirm the picture and add quantitative detail. A valuable qualitative addition that hyperquenching studies might possibly make, concerns the secondary or $\beta$-relaxation, the relation of which to the $\alpha$-relaxation is not so well understood. There is reason [13] to believe that, between the normal glass transition and the crossover temperature $T_x$, this secondary process becomes rapidly stronger [13,15] as documented for sorbitol [25] such that, by $T_x$, it becomes the dominant relaxation process. Hyperquenching studies may help us confirm and understand, or alternatively refute, such a significant inversion.

Although the glass transition is usually observed and recorded during heating experiments, it is more rationally defined during cooling experiments and certainly it is the cooling glass transition that is of interest in hyperquenching experiments. Because the numerical value of the glass transition during rapid cooling must be obtained by studies made after the glass has been formed, it is usually referred to by a distinct name, the ‘fictive’ temperature [26]. In the simulation community, the alternative term ‘internal’ temperature is also used [5–8], though the latter is also defined from the behavior of the glass below $T_m$, rather than estimated by the method of this, and related, papers. Velikov et al. [27] have shown that the fictive temperature and the midpoint cooling glass temperature are almost identical in value, at least for single component systems.

The process of maintaining full equilibrium in a liquid (excluding crystallization if this is a possibility) involves the exploration of the potential energy ‘landscape’. So also does the process of approaching equilibrium. For equilibrium to be established, the system point must move between a large enough subset of the basins at the appropriate level on the landscape effectively to have explored them all. What is happening during this exploration that is needed to achieve the equipartition of kinetic and potential energy? Clearly the degrees of freedom must communicate. There must be an exchange of energy between the phonon and configuron microstates of the system. At equilibrium, the forward and reverse exchange rates between these microstates must be the same. Otherwise the system is said to be annealing, and its properties are time-dependent. Likewise, when the phonon-configuron exchange, which is responsible for maintaining equilibrium during cooling, becomes too slow, then equilibration fails and the system becomes non-ergodic, as in glass formation.

The energy of the basin in which the system becomes trapped during continuous cooling is higher the higher the cooling rate. The potential energy of the trapped state can be depicted for different cooling rates, as in Fig. 3 of Ref. [2], in which the fictive temperatures are also indicated. Note that $T_f$ relates to potential energy while the ‘real’ temperature relates to kinetic energy. When the two temperatures are the same, the system is a liquid. Otherwise it is a glass.

While fictive temperatures often can be determined by observations made during cooling, this becomes difficult or impossible when the cooling rate are high. Then the fictive temperature can be assessed by calorimetric measurements performed on the quenched glass during its reheating, as described in detail in recent papers [1,3] which relate back to early studies by Moynihan and coworkers [28]. We will illustrate these features in the present work in which we report on the adaptation of the electrospray technique for differential scanning calorimetry studies of the hyperquenched glassy systems. We adopt the much-studied glassformer 1,2-propanediol (propylene glycol, PG) as our trial substance and use the data obtained to show how features of the potential energy hypersurface,
that are not obvious from ergodic measurements, can be revealed.

2. Experiment

Much attention has been given to different methods of quenching liquid systems at high rates, mostly for the purpose of vitrifying liquid metals or refining the grain size of crystalline materials [29], but no review will be given here. A technique that has been utilized for the above purpose, but which has also been used to produce finely divided systems (including those containing proteins) for mass spectrometric analysis, is that of electrospraying [30]. In this technique, a metered flow of liquid self-subdivides into very fine droplets, as it emerges from a fine needle orifice, under the mutual repulsion of electrons that are driven onto the liquid surface by a high electrostatic field. It can be refined to the point where even liquid silicon can be obtained as vitreous droplets [31]. It is much used for sample preparation in mass spectroscopy. It is extremely well suited for producing small samples of liquids sprayed directly into cold pans in the dry environment of the typical differential scanning calorimeter sample housing, and it has therefore been the technique adopted by us for hyperquenching studies.

The experimental set-up is shown in Fig. 1. The 1.0 ml capacity syringe, driven by controlled rate stepper motor, supplies liquid through a short length of 0.030" × 1/16" peek tubing and adaptor to a 0.004" × 0.009" stainless steel needle. The adaptor inserts through the upper perspex plate of the DSC sample head dry box. It inserts directly over an aluminum sample pan that sits on a cold aluminum support rod in contact with liquid nitrogen which is funnelled into the mini bath shortly before spraying is to commence. High voltage is applied between the aluminum rod and the syringe needle, the latter contact being simply accomplished by having the syringe needle drop through the splayed end of a multifilament wire lead secured to the dry-box housing.

The voltage, controlled between 6000 and 15000 V, was supplied by a home-made power supply designed to have maximum current flows that are non-hazardous on direct contact. Voltages higher than 12000 V produced corona discharges in the dry box atmosphere of N\textsubscript{2}. This arcing can be suppressed in a CO\textsubscript{2} atmosphere [32] and this will clearly be needed in order to spray high surface tension aqueous systems satisfactorily [33]. The steady flow of liquid, which is an important control parameter [30], was provided by a stepper-motor-driven syringe, the step rate itself being under precise control. The flow rates found best are in the range of 3–15 µl/min.

Each liquid sprays optimally under different voltage and flow rate conditions – which must be determined empirically. While we have not yet electrosprayed water effectively, we find that the lower surface tension, but still hydrogen-bonded, liquid propylene glycol, has very satisfactory electrospraying characteristics, and we use it for our initial studies.

To utilize the hyperquenched samples for study of the quenched-in state, and its relaxation to the normal state, we compare the thermal behavior of the hyperquenched sample with a ‘standard scan’ of the same sample. The standard scan [1,27,34] is one in which the heat flow is measured during an upscan at the standard scan rate of 20 K/min after preparing the sample initially by cooling it

![Fig. 1. Experimental set-up for electrospraying small samples into cold DSC pan inside dry-box of DSC. Samples are prepared by successive bursts of droplets, allowing time for the first deposit to regain the pan temperature before the next arrives.](image)
through the glass transformation range at 20 K/min. For the comparison, the quenched sample is upscanned at the standard rate, and the two scans are superposed using the data at temperatures (i) below that of the relaxation onset of the quenched sample, and (ii) above the glass transformation range, \( T > 1.1 T_g \), (where all traces of the sample history disappear) to adjust any slope discrepancies.

3. Results

In Fig. 2 we compare standard scan and quenched sample scans for two cases quenched at two different rates. The upper pair of curves is for a sample that was initially quenched by dropping it, in a hermetically sealed aluminum pan, into a bath of liquid nitrogen, before cold transfer to the DSC head for upscan. The lower pair is for a sample that was electrosprayed into an open DSC pan, as described in the previous section, before cold transfer to the DSC head. The difference between the energies trapped in the two cases is immediately seen, by the much larger area lying between the standard scan and the quenched scan in the case of the electrosprayed sample.

The effect of changing the cooling rate, under instrument control, between 5 and 40 K/s on the scans for propylene glycol can be seen in Fig. 3. At these much lower cooling rates the difference between standard and non-standard scans is seen mainly in the immediate vicinity of the glass transition, whereas in the case of higher quench rates the difference is manifested at increasingly lower temperatures. The origin of this distinction will be discussed in the next section.

Fig. 3 is used to obtain the data needed to estimate the quench rate from the data of Fig. 2. The way in which the areas between standard scan and scans at other non-standard rates can be used (see Fig. 3 inset) to obtain the fictive temperature \( T_f \), used in the Fig. 4 plot, is obtained in each case.

In Fig. 4 we show data for the second liquid of this study, di-\( n \)-butylphthalate, DBP. Fig. 4 shows the standard scan for DBP, and compares it with the results of two scans of glasses that were initially hyperquenched. This scan resembles that of the hyperquenched PG, but does not show as large an effect, primarily because it is a more

![Fig. 2. Comparison of the upscan (at standard scan rate) of quenched samples with standard samples for the case of propylene glycol. The upper pair is for a sample, in sealed pan, dropped into liquid nitrogen, while the lower pair is for electrosprayed sample in open pan. The much larger frozen-in enthalpy of the lower case is seen in the much larger area between the two scans for this case.](image1)

![Fig. 3. Upscans of samples cooled under instrument control at different rates, including standard rate of 20 K/min, (left hand ordinate) and the differences between standard and non-standard scans (right hand ordinate, lower curves). The insert shows how the fictive temperature \( T_f \), used in the Fig. 4 plot, is obtained in each case.](image2)

![Fig. 4. Twenty K/min scan of standard dibutyl phthalate glass (dashed line) compared with upscan of hyperquenched glass after annealing for 90 min at 151 K. Note the annealing pre-peak which has developed while the slow part of the excess enthalpy remains unaffected on this time scale. Note that the prepeak departs from the baseline only at temperatures far above the annealing temperature of 151 K.](image3)
3.1. Data treatment

The fictive temperatures obtained are plotted in a reduced form in Fig. 5. The slope (and intercept) of this plot both yield the liquid ‘$m$ fragility’ [35] or ‘steepness index’ [36], with a precision which is not exceeded by that of any other technique, as recently documented in detail [34]. The value of $m$ obtained from Fig. 5 is 54, whereas that reported on the basis of dielectric relaxation measurements in Ref. [37] is 54 and that tabulated in Ref. [35] from ac specific heat data [38] is 52.

The data of Fig. 5, guided by the form of the dielectric relaxation temperature dependence [37] which is shown as a dashed line in Fig. 5, can now be used to estimate the hyperquenching rate. This is obtained from the intersection with a vertical line representing the scaled fictive temperature obtained for the hyperquenched sample, by the same area integration method. The fictive temperature is found to be 195 K, or 1.15 $/C_0$, with a precision which is not exceeded by that of any other technique, as recently documented in detail [34].

The fictive temperature obtained from Fig. 2 (upper curves) is only 8.5 K above the standard value of 169 K and this yields, from Fig. 5, a quenching rate of only 120 K/s. Nevertheless, this is a useful quenching rate for some purposes, being 24 times faster than the fastest quench obtainable in the DSC itself (5 K/s). For instance, we have used it to completely suppress the refolding of denatured lysozyme during vitrification, prior to carrying out novel controlled refolding studies [40].

4. Discussion

4.1. Calorimetric quantification of initial trap energy level

Using the data of Fig. 2, we can now proceed to estimate the energy, and depth, of the trap in which the sample was arrested during the hyperquench at $10^5$ K/s. The energy of the trap minimum relative to that for the trap in which the standard glass resides, has already been obtained in finding the fictive temperature. This energy gap, given by the area between the hyperquenched and standard scans of Fig. 2, amounts to 1.9 kJ/mole. This is not a useful figure without some relevant scale of energies to which to refer. The most relevant comparisons are with (a) the enthalpy of fusion (b) the enthalpy of exciting the liquid from the glass temperature to the melting point and (c) the enthalpy of exciting the liquid from the Kauzmann temperature to the boiling point. The value of (a) is not available for 1,2-propanediol, which is extremely difficult to crystallize, but is known for the 1,3 isomer for which it is 12.9 kJ/mol. The value for the 1,2-isomer, when measured, will be similar but smaller: we estimate 12.6 kJ/mol. The values of the enthalpies (b) and (c) can be estimated from the relations

$$\Delta H = \int_{T_e}^{T_m} \Delta C_p dT$$

and

$$\Delta H = \int_{T_k}^{T_b} \Delta C_p dT.$$  

The respective values are 3.69 kJ/mol, and 25 kJ/mol. The latter, which is only approximate for the reasons given below, can be taken as a crude measure of the ‘height of the energy landscape’ for the system, which is conceptually simplest for a constant volume system. The relation between excitation at constant volume ($C_v$) and excitation...
at constant pressure has \((C_p)\) been considered recently [41,42], and it is clear from such considerations that Eq. (2) will overestimate the height of any fixed volume landscape. The overestimate contains three components, none of which will be as important for PG as for most other molecular liquids.

The first component is due to the higher heat capacity at constant pressure over the value at constant volume for which the landscape, and its inherent structures excitation profile, is defined [14]. The extra heat capacity \((\Delta C = \gamma VT/\Delta T^2)\), inflates the integrand, but since the expansivity of PG is among the lowest measured for molecular liquids, while the compressibility is normal, the effect will be small.

The second component is due to the changes in the basin shapes that usually occur with level on the landscape, and these changes lead to an excess heat capacity over that due to the configurations alone. The excess is a positive quantity at \(C_p\) and negative by about the same amount at \(C_v\) [42-45]. Again, it is expected that this source of difference is quite small for the case of PG which is not a very fragile liquid, as seen above.

The third component comes from uncertainty about the course of \(\Delta C_p\) (or \(\Delta C_v\)) above the melting point. It is expected to decrease and eventually to become undefinable as the lifetime of the ‘structure’ becomes comparable with vibrational time scale. Our estimate has assumed the almost constant value of 72.5 J/mol K observed in the range \(T_g - T_m\).

Taking all these factors into account, we can take the height of the landscape for PG, with a volume fixed at its value at the glass transition, to be about 20 kJ/mol.

Then we can see that, notwithstanding the seven orders of magnitude increase in quenching rate that we have imposed, the energy trapped in the hyperquenched glass in excess of the energy of the standard glass, is rather small relative to the height of the landscape. It is even small relative to the part of the landscape explored between \(T_g\) and \(T_m\). This reflects the fact that these seven orders of magnitude lie in the regime in which the relaxation time is changing most rapidly with the enthalpy, and accordingly correspond to a relatively small enthalpy change. A change in the quench rate by the same number of orders of magnitude in a computer simulation experiment would involve the system in much larger changes of potential energy because of the relatively larger distance from the Kauzmann temperature in which such a change is being made.

4.2. Calorimetric characterization of the initial trap depth

The depth of the basin in which the system is trapped during hyperquenching is a more interesting quantity. It can be estimated in two independent Ways from the data obtained in this study. Firstly, it can be estimated from the temperature at which the trapped-in enthalpy starts to be released during the rescan, assuming that the probability of escape from the trap is a Boltzmann function of temperature. Secondly, it can be estimated from the fictive temperature with the help of assumptions about the ‘true’ activation energy for rate processes in viscous liquids. For PG, it is found that both approaches lead to the same trap depth.

In the first approach [2] we use the fact, based on experience with the glass transition, that when an energy change first commences (at the onset glass transition) during a standard scan (20 K/min), the relaxation time for the energy-changing process is 100 s. The energy of the barrier opposing the relaxation can then be obtained by supposing a Boltzmann probability, \(\exp(-E_{\text{esc}}/RT)\), of escaping from the trap at the temperature \(T_{\text{esc}}\), and a pre-exponent time constant of \(10^{-14}\) s, based on lattice vibrations.

Thus we can write

\[
100 \text{ s} = 10^{14} \text{ s} \exp \left( \frac{-E_{\text{trap}}}{RT} \right),
\]

from which

\[
E_{\text{trap}} = 2.303RT_{\text{esc}} \log(10^{16}) = 37RT_{\text{esc}}.
\]

The trap depth for the present case of hyperquenching, in which \(T_{\text{esc}} = 125\) K, is then 39.9 kJ/mole, an energy very much larger than the energy separating the excited glass from the normal glass, as calculated above (1.9 kJ/mol).

Before discussing this value further, we consider the alternative method of assessing the trap depth. We argue, following Dyre [46] that, at the fictive temperature, \(T_f\), located at 1.15\(T_g\), the true activation energy for migration should be given by the construction in which the distorting effect of change of structure with temperature has been removed. Thus, instead of taking the actual slope of the Arrhenius plot for the relaxation time in Fig. 6, the energy barrier opposing the rearrangement of molecules in viscous flow is taken as 2.303R times the slope of the straight line through the fictive temperature to the lattice vibration time, \(10^{-14}\) s. This yields 39.1 kJ/mole for the trap depth, which is very close to that from method 1. Indeed this accord can be seen immediately from the manner in which the extrapolation of the straight line through the fictive temperature to the time \(\tau = 100\) s, yields the temperature 125 K where relaxation begins in Fig. 2.

4.3. Interpretation of the trap depth

The self-consistency of these assessments of the trap depth prompts a series of further questions. For the slower (liquid nitrogen pan immersion) quench (upper plot in Fig. 2) the trap depth should be greater. Using the fictive temperature (again obtained from the total energy evolved) to obtain the activation energy, we would predict from Fig. 6 a recovery onset temperature of 150 K. The onset temperature in Fig. 2 is not as well-defined for this case, but there is clearly some weak relaxation below 150 K. This
may be due to the spreading out of the relaxation time distribution, which is known to increase with decreasing temperature.

At the glass temperature itself (i.e. at the fictive temperature of the ‘standard’ glass) the activation energy for enthalpy relaxation is obtained as 52 kJ/mol, which is close to the enthalpy of vaporization ($\delta H_v = 56.7$ kJ/mol) at the boiling point of 460.5 K [47]. Before further comment on this correspondence it is helpful to make some comparison with rate processes in other hydrogenbonded systems, preferably other molecules with two H bonding units per molecule. For instance, the activation energy for diffusion of water molecules in ice [48], which is an Arrhenius process, is 58.5 kJ/mol. This value, which is also obtained for dielectric relaxation, NMR spin-lattice relaxation, and elastic relaxation [48], is greater than the enthalpy of vaporization, 40.66 kJ/mol at the boiling point of water. A more appropriate comparison is with the sublimation energy which is 51 kJ/mol [49,50]. The sublimation energy provides the major component of the derived lattice energy of ice, 56 kJ/mol according to Whalley [49,51].

That the energy fluctuation needed to permit a single particle process like diffusion in a molecular crystal should be comparable to the lattice energy, should cause no surprise. It seems reasonable because the relevant fluctuation involves the expenditure of energy in deforming the lattice sufficiently that a molecular size void is both available and accessible (written as the product of Boltzmann probabilities for void formation and for ‘jumping’ into the void). The manner in which a similar energy fluctuation in an amorphous substance gives rise to diffusion, and thereby to relaxation ($\tau \approx d^2/6D$, where $d$ is the diameter of the rearranging entity, and $D$ is the self-diffusion coefficient) is, on the other hand, not so clear. It is generally believed, after Adam and Gibbs [52] that many particles cooperate in the process and that in this manner the necessity for a molecular sized cavity is avoided. Whatever the detailed mechanism may be, it does not seem surprising to the present authors that, near the glass temperature, the energy fluctuation involved should be comparable to that needed for diffusion in crystals. After all, at the glass temperature, (a) the activation energies for processes at constant volume and constant pressure have become essentially the same [42,53], and (b) the self-diffusion coefficient is smaller than has so far been measured in any crystalline substance except silicon [54]. Indeed, the measurement of such a slow diffusion process in solids was only achieved fairly recently [55–57].

Fig. 6. Assessment of the activation energy for relaxation from the fictive temperature, $T_g$, and the prediction of the temperature at which a glass of this fictive temperature will start to relax during warm-up at the standard DSC heating rate of 20 K/min, i.e. the temperature where the relaxation time will have the value of 100 s. Here the standard fictive temperature ($T_g^s$) is the fictive temperature of the glass that has been cooled at 20 K/min, and is numerically within 0.5 K of the common midpoint heating glass temperature, $T_g$. The two open circles are the fictive temperatures determined by calorimetry, using Figs. 2 and 5, for the electrosprayed, and the liquid nitrogen quenched samples, respectively. Straight lines through the fictive temperatures correctly predict.

4.4. Energy landscape considerations

These considerations have some bearing on the way one must think about energy landscapes. Since the landscape has $3N+1$ dimensions and a number of minima of the
order of \( \exp(N) \), there are difficulties in discussing its features directly. It is easier to think first of the landscape for the crystal. Here it is clear that a mechanically stable minimum on the configuration space landscape corresponds to a real space lattice containing a specified number of defects. To move up to a higher level on the landscape it is necessary to create additional defects. In order to change from one basin to another it is evidently necessary to surmount a barrier (the known single particle diffusion activation energy) which is always far above even the highest ‘basins’ of the landscape, and which approaches the lattice energy in magnitude. This is the common barrier concept invoked by Brawer, [59] and Dyre [46], and most recently utilized in the dynamic Gaussian excitations model of Matyushov and Angell [60]. ‘Landscape’ is perhaps too gentle a description of such an energy topography.

The question to be answered in connection with liquids is the extent to which a similar situation applies to liquid landscapes under conditions where energies and diffusivities approach those of the crystal. At high energies, according to simulations, the landscape broadens out to a high plateau and the most common ‘basin of attraction’ [23] (above which the system ‘floats’) is of small depth and high anharmonicity [14,58]. It is often written that such minima can be reached from any other minimum without the need to cross significant barriers, there being many directions with low energy saddles. At lower temperatures significant barriers emerge [61]. A question provoked by our observations is whether the liquid landscape evoked by the simulations remains completely distinct from the crystalline case, or whether indeed its fate, at low energies, is to become as difficult to explore as that of the crystal.

4.5. Shadow glass transitions

A rationale for carrying out studies of the hyperquenched states of easy glassformers is that such studies permit a direct comparison with the properties of the same system vitrified on leisurely time scales. Most previous observations on the behavior of glasses of very high fictive temperatures have been made on metallic glasses which are complex mixtures of metals and it has not been clear whether the unusual annealing effects, such as the development of small endotherms like miniature glass transitions in successive stages, depending on annealing temperature, can be examined. When a glass has been created suddenly, by increases in pressure, a similar annealing series can be seen. Such stages in the relaxation of HDA (high density amorphous water), were recently reported [66] but were interpreted as evidence for different distinct polymorphs of water.

5. Concluding remarks

By controlled annealing studies such as those recently reported for a hyperquenched mineral glass [3], the manner in which the hyperquenched glass descends the landscape in successive stages, depending on annealing temperature, can be examined. When a glass has been created suddenly, by increases in pressure, a similar annealing series can be seen. Such stages in the relaxation of HDA (high density amorphous water), were recently reported [66] but were interpreted as evidence for different distinct polymorphs of water.

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[51] Pursuing this thought, we obtain a major part of the quasi-lattice energy" for the PG glass by adding the height of the landscape estimated above (20 kJ/mol) to the vaporization energy at the boiling point (56.7 kJ/mol) to obtain the approximate value 77 kJ/mol.