

# Lecture 6

9/9

Today : "Energy budget" in Hw1

↳ Task 3

Recap (Lec 5)

Mass eq. (continuity eq.)

Fully compressible flow:

$$\text{An eq. of density} \quad \frac{\partial \rho}{\partial t} = - \left( u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) - \rho \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)$$

Fluent → "Density based solver"

Incompressible flow ( $\frac{d\rho}{dt} = 0$ ), (special case:  $\rho = \text{const.}, \text{Hw1}$ )

$\rho$  vanishes entirely

$$0 = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \quad \text{implies}$$

$$\nabla \cdot \vec{V} = 0 \quad \text{--- (1)}$$

Fluent → "Pressure based solver"

1

Energy Eq. (1st law of thermo.)  $\rightarrow$  should be

$$\cancel{\frac{dq}{dt}} = \cancel{s_p} dT + \cancel{pdv} - V dp$$

(this doesn't affect the rest of discussion)

Hw 1 (No heat source/sink)

$$s \equiv \text{const}$$

— (2)

$$\frac{dT}{dt} = 0$$

L

E

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = 0$$

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = 0$$

— (2\*)

Correction:



$$\frac{\partial T}{\partial t} = - \nabla \cdot (\vec{v} T)$$

———

(3)

$$0 = \nabla \cdot \nabla$$

$$\frac{2e}{Te} =$$

Total thermal Energy for the whole system in  $Hw\ 1$

(internal) → correction:  
should be  
"enthalpy"

$$E \equiv \iiint_V c_p \cdot g \cdot T \, dV$$

~~$$\frac{dE}{dt} = \frac{d}{dt} \iiint_V c_p \cdot g \cdot T \, dV$$~~

Steady  
sol.

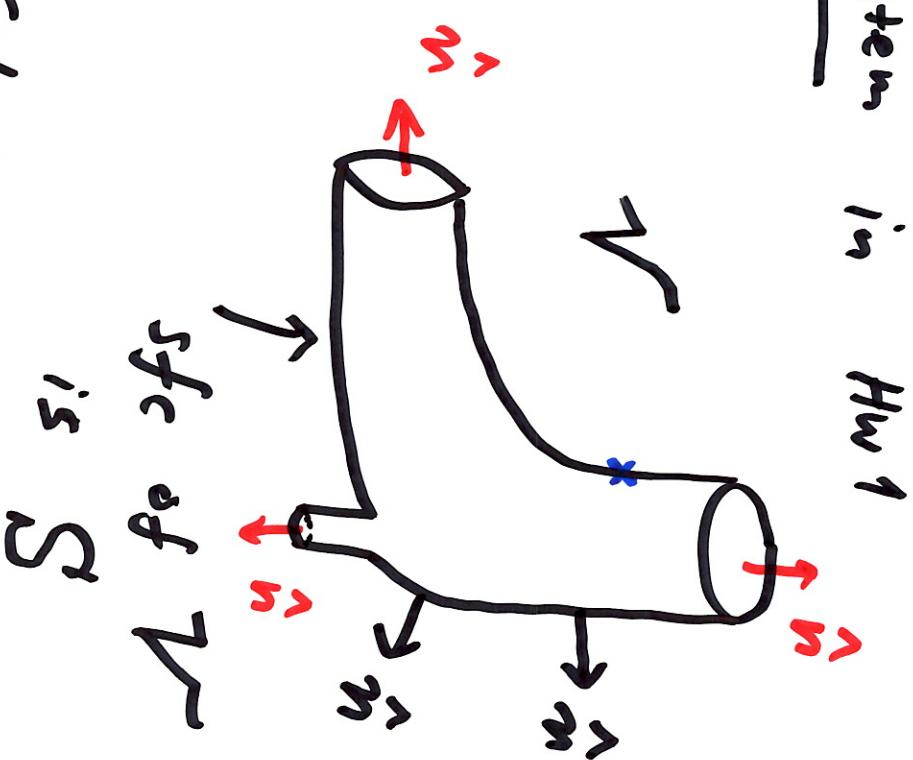
$$= c_p \cdot g \cdot \frac{d}{dt} \iiint_V T \, dV \quad \text{calculation}$$

$$= c_p \cdot g \iiint_V \frac{\partial T}{\partial t} \, dV$$

$$\text{Energy eq.} \rightarrow = -c_p \cdot g \iiint_V \nabla \cdot (\vec{v}_T) \, dV$$

div.

$$\text{Gauss} \rightarrow = -c_p \cdot g \iint_S (\vec{v}_T) \cdot \hat{n} \, dS$$



$$c_p \cdot \rho \oint_S (\vec{v} \cdot \vec{T}) \cdot \hat{n} dS = 0$$



$$g_I \equiv \iint_I c_p \cdot \rho \cdot v_n \cdot T dS$$

$$g_{II} \equiv \iint_{II} c_p \cdot \rho \cdot v_n \cdot T dS$$

$$g_{III} \equiv \iint_{III} c_p \cdot \rho \cdot v_n \cdot T dS$$

We anticipate:

$$g_I + g_{II} \approx g_{III}$$

Small discrepancy due to num. error

HW 1 - Task 3

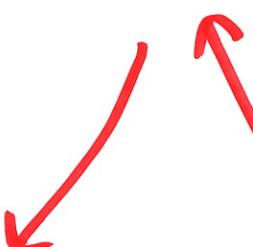
Another source of discrepancy :

$$g_I + g_{II} \approx g_{III}$$

we ignore molecular heat conduction  
(which is INCLUDED in filament)

$$\frac{\partial T}{\partial t} = - \nabla \cdot (\vec{V}T) + \kappa \nabla^2 T$$

=



$$\cancel{\frac{dE}{dt}} =$$



...

$$\underbrace{\int \int \int}_{g_I, g_{II}, g_{III}} - \nabla \cdot (\vec{V}T) dV +$$

$$\boxed{\text{extra}}$$

$$g_{IV}$$

For MW1,  
it's very  
small

Impose  
backflow

T  
back?

outlet



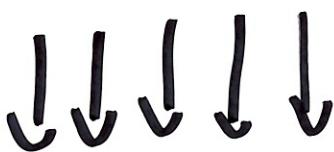
Computing  $\mathcal{G}_I, \mathcal{G}_{II}$ :

Simple:  $u_{inlet} \text{ const}$

$T_{inlet} \text{ const}$

$$u = 0.4$$

$$\frac{u}{L}$$



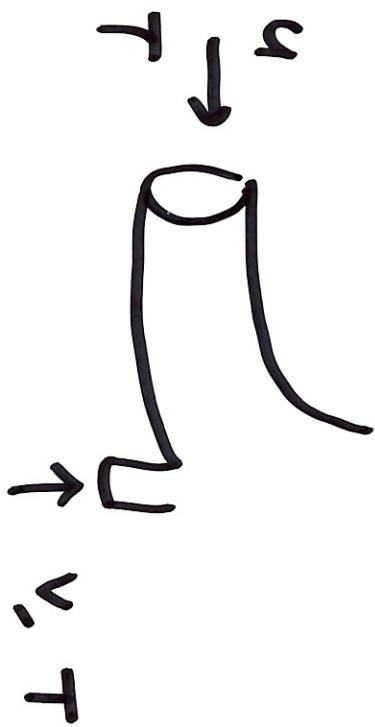
$$T_e = ? \cdot \kappa$$



$$\iint_I u T dS$$

$$= u \cdot T \cdot (\text{area})$$

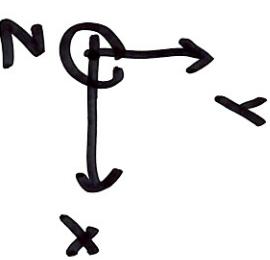
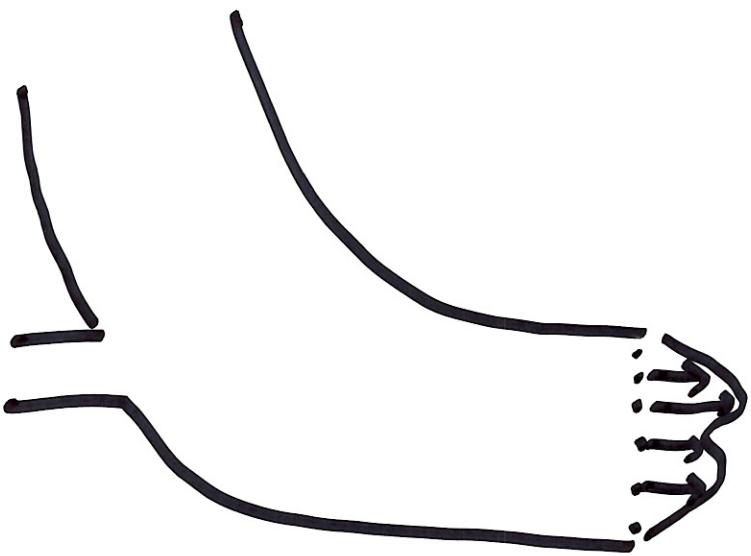
Fluent  
Mesh w/ finite  
resolution



$u(x, z)$

$T(x, z)$

$$\iint_{\text{III}} u(x, \dots) T(x, \dots) dS$$



$$\iint_{\text{IV}} u dS$$

Fluent:

Step 1: Define

$$F \equiv u \cdot T$$

Step 2:

Surface Integral

Custom Field Function  
(Tutorial #2)

## \* Convergence criterion

## Convergence criterion

**Residual  
(Scales)**

Steady sol.

**Fluent :** Iterations

$$\text{e.g.: } \left\{ \begin{array}{l} \square + \square + \square = \\ \square + \square = \end{array} \right. \quad \left. \begin{array}{l} \square \\ \square \end{array} \right\}$$

四

$$x^2 + x = 3$$

1st iteration

$$x = 2$$

1st iteration  $x = 2$   
2nd iteration  $x = 1.5$

$$= 2 \cdot 2 + 2^2$$

七八

卷之三

$$(1.5)^2 + 2$$

225

卷之三