Nicholas Fette Update for Phelan lab group meeting

Outline

- 1. Interesting news from the world
- 2. Waste heat utilization (AORA Solar)
- 3. Dissertation outline (most recent)
- 4. Social ideas

H. J. Cho, J. P. Mizerak and E. N. Wang, "Turning bubbles on and off during boiling using charged surfactants," *Nat Commun*, vol. 6, no. 8599, pp. 1-7, 2015. http://dx.doi.org/10.1038/ncomms9599.

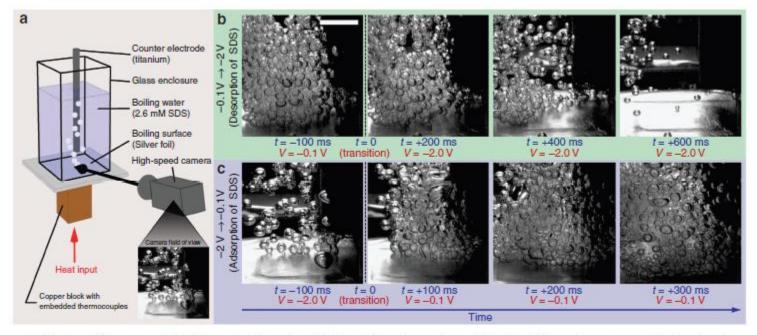


Figure 1 | Turning boiling on and off with a potential switch. (a) Pool boiling of a solution of 2.6 mM SDS (negatively charged) in DI water at a constant heater power of 60 W with potential applied between the silver foil boiling surface and an immersed titanium counter electrode. A (b) -0.1 to -2.0 V switch decreased bubble nucleation within 600 ms due to electrostatic desorption of SDS from boiling surface. A (c) -2.0 to -0.1V switch increased nucleation within 300 ms due to adsorption of SDS (see Supplementary Movie 1). Scale bar, 1cm.

H. J. Cho, J. P. Mizerak and E. N. Wang, "Turning bubbles on and off during boiling using charged surfactants," *Nat Commun*, vol. 6, no. 8599, pp. 1-7, 2015. http://dx.doi.org/10.1038/ncomms9599.

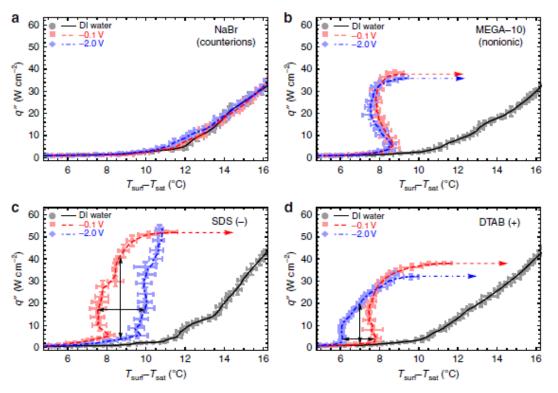
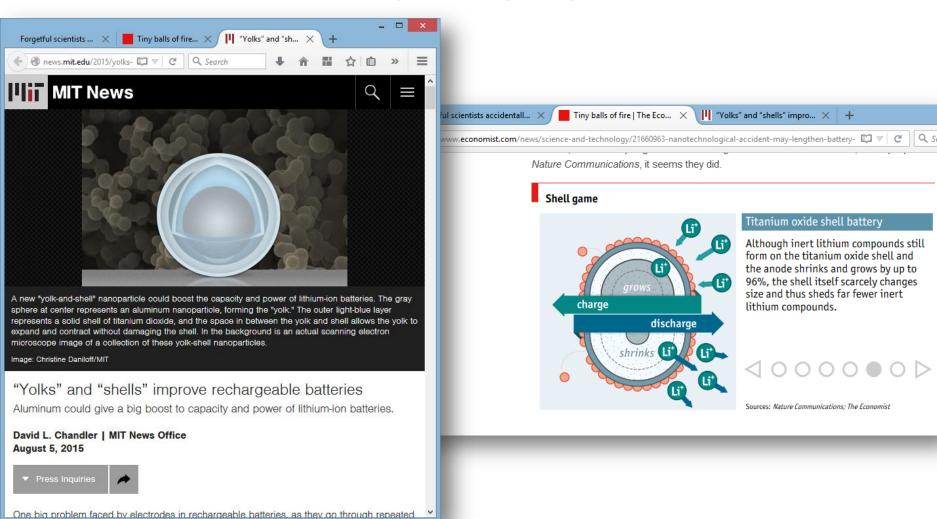


Figure 4 | Boiling curves showing tunability of charged surfactants. Plain DI water (black), -0.1V (red) and -2.0V (blue) boiling curves for 2.6 mM (a) NaBr, (b) MEGA-10, (c) SDS and (d) DTAB. Time averaged data points from an individual boiling experiment with error bars (2 standard deviations in data spread from time averaging) and moving averages (lines) are shown. Boiling was not affected by voltage for (a) NaBr and (b) MEGA-10. For (c) negatively charged SDS, the boiling curve at -2.0V was right-shifted with higher CHF compared with -0.1V. For (d) positively charged DTAB, the boiling curve at -2.0V was left-shifted with lower CHF compared with -0.1V. The maximum change in HTC (tunability) at constant q'' (horizontal arrows) and constant superheat (vertical arrows) are shown for SDS and DTAB.

Fun news



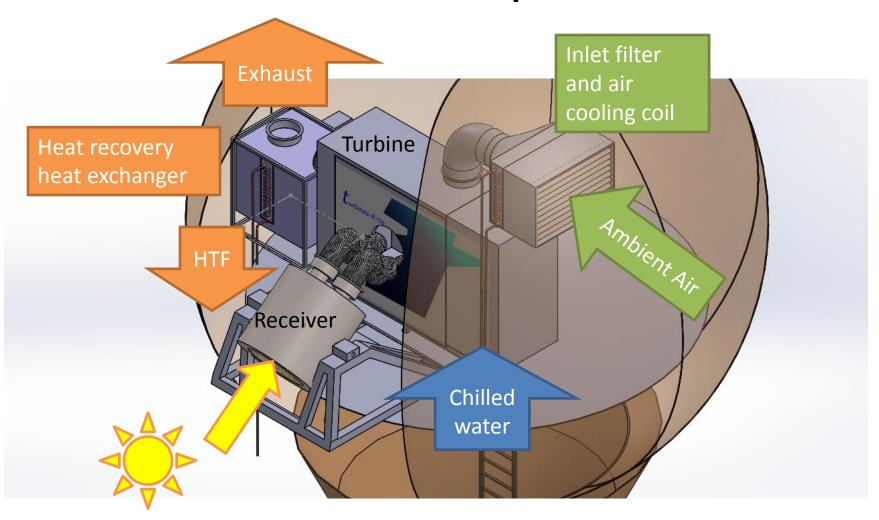
AORA Solar collaboration

- Pinchas Doron
 - AORA
- Ellen Stechel
 - Nathan Johnson
 - Marcus Herrman
 - Yulia Peet
 - Clark Miller
 - Perdo Peralta
 - Pat Phelan

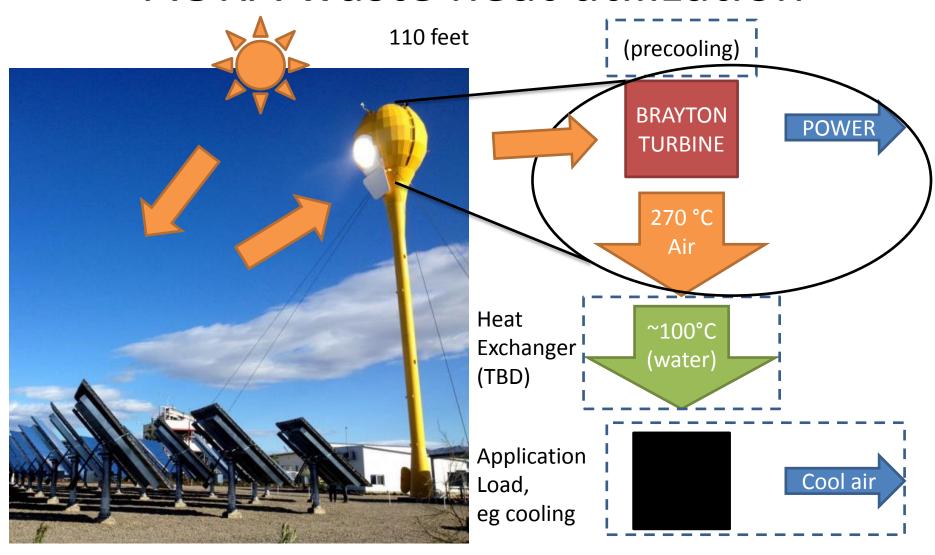


J. M. Duran, "AORA Solar's Tulip System: A hybrid solar thermal solution," 25 11 2013. [Online]. Available: http://www.iitj.ac.in/CSP/material/21dec/aora.pdf. [Accessed 02 11 2015].

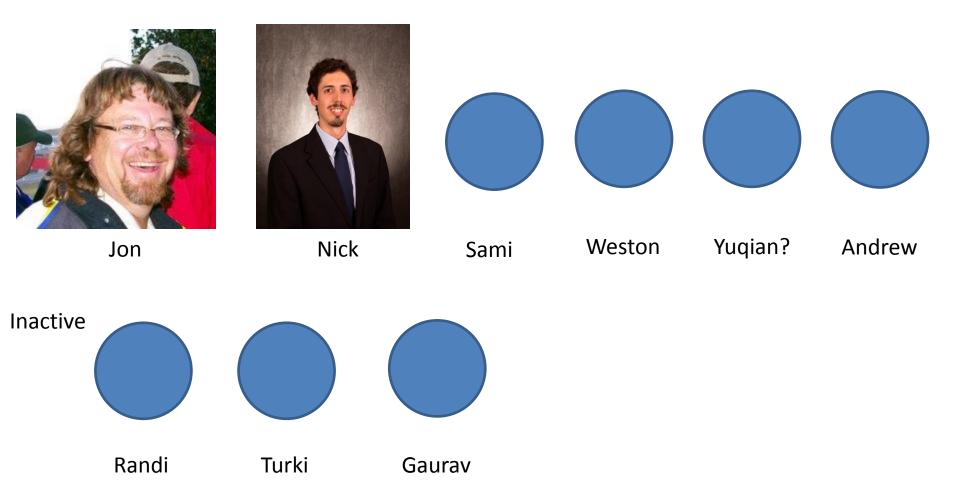
Close-up



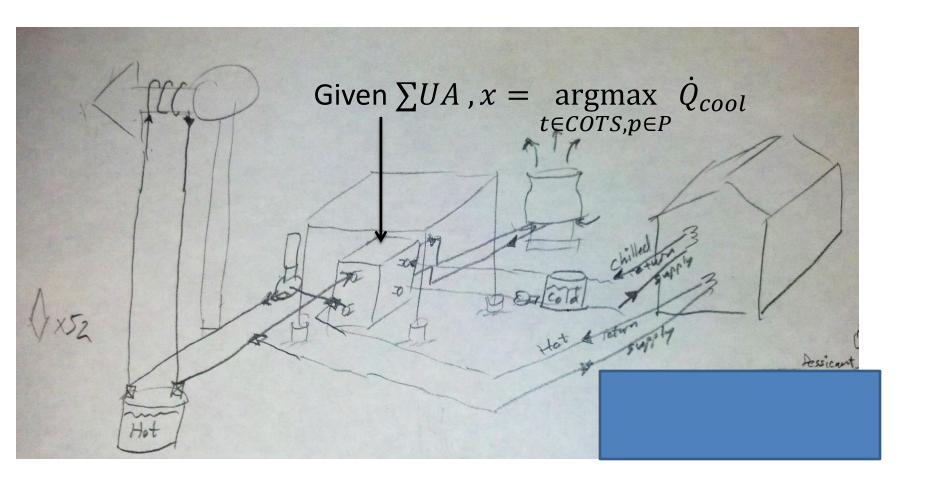
AORA waste heat utilization



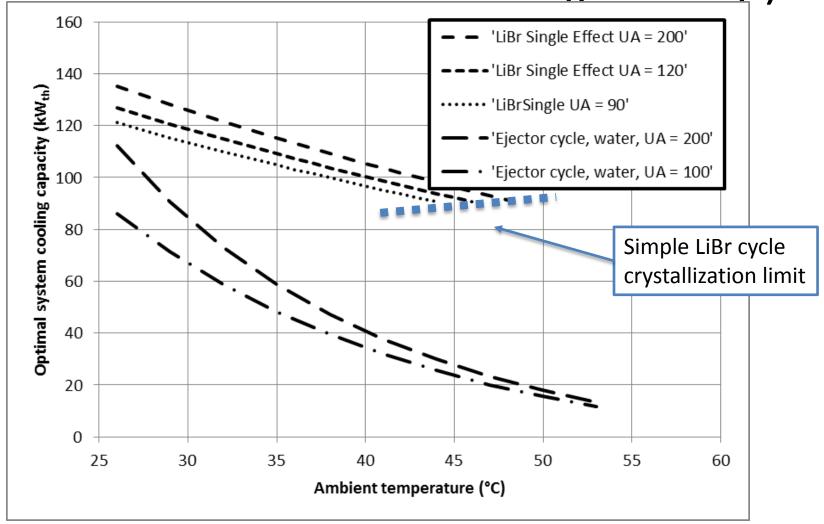
Waste heat utilization team



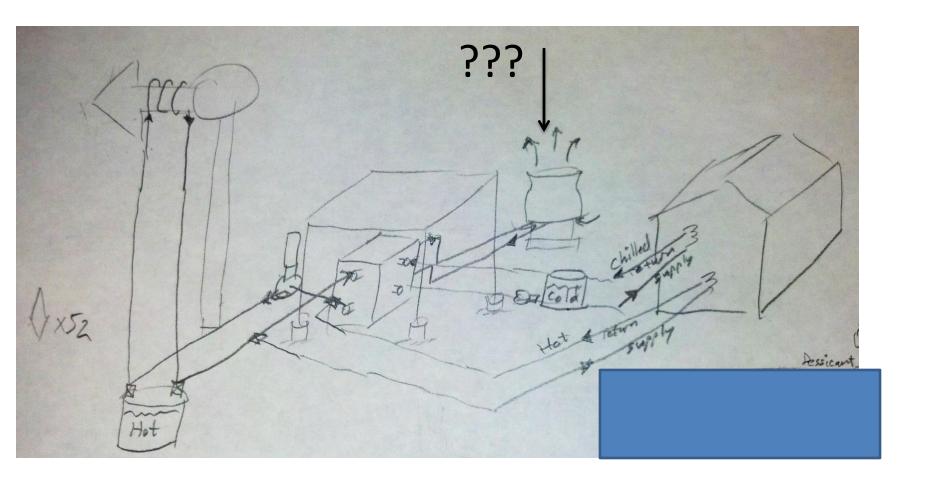
Nick's dissertation Chapter 1



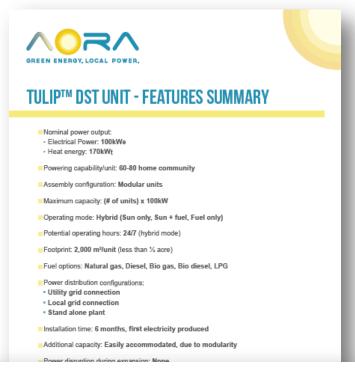
Cooling technologies compared that deliver 10 °C chilled water (per Tulip)



Nick's dissertation Chapter 2



Existing spray cooling system





Operational water use: Minimal; 230 I/MWh (when temperature is above 35°C)

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Options for use of available heat:

Space heating
Refrigeration
Air conditioning
Water desalination
Assistance for bio-gas generation

J. M. Duran, "AORA Solar's Tulip System: A hybrid solar thermal solution," 25 11 2013. [Online]. Available: http://www.iitj.ac.in/CSP/material/21dec/aora.pdf. [Accessed 02 11 2015].

AORA Solar Ltd., "Tulip Datasheet," 07 11 2012. [Online]. Available: http://aorasolar.com/wp-content/uploads/2012/01/DatasheetInfographic-MedRes.pdf. [Accessed 02 11 2015].

Heat rejection: evaporative technologies

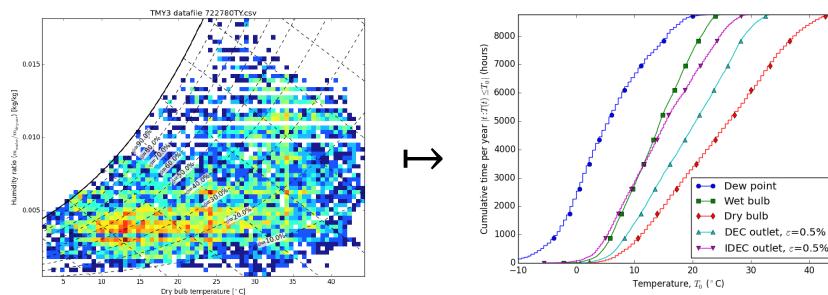


Figure 29. Probability distributions of ambient conditions calculated from TMY3 data for Phoenix [40].

Figure 1. Probability distributions of some effective temperatures calculated from TMY3 data [30] for dry bulb and dew point, including direct evaporative cooler (DEC) and indirect evaporative cooler (IDEC).

30

40

Heat rejection: evaporative technologies

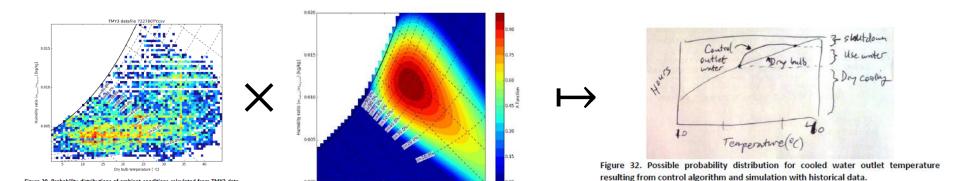


Figure 29. Probability distributions of ambient conditions calculated from TMY3 data

for Phoenix [40].

Heat rejection

Table 1-3
Tradeoffs Among Various Types of Cooling Systems

Tradeoff	Cooling System Type						
	Once-Through	Wet Mechanical Draft	Dry Air-Cooled Condenser	Hybrid Wet/Dry			
				Plume Abatement	Water Conservation		
Water Consumption	Minor	8 to 12 gpm/MWe	~ 0 to <5% of wet tower	~ equal to wet tower	20% to 80% of wet tower depending on design		
Capital Cost	<< BASE	BASE	1.5x to 3x base	1.1x to 1.5x base	3x to 5x base		
O&M Cost	< BASE Pump maintenance, condenser cooling	Highly site specific; fan/pump power; water treatment; tower fill/ condensate cleaning	Finned surface cleaning; gearbox maintenance; fan power	Similar to BASE	Similar to BASE		
Performance Penalty	< BASE Base penalty depends on site	BASE	Highly site specific—5% to 20%	~ Equal to base	Highly variable, depending on mode of operations		

J. S. Maulbetsch, "Comparison of Alternate Cooling Technologies for California Power Plants: Economic, Environmental and Other Tradeoffs: Consultant Report," EPRI, California Energy Commission PIER, Atherton, CA, 2002.

Heat rejection

6.1. Hybrid ratio

Hybrid ratio is defined as the ratio of the heat that must be removed in dry section to the total cooling load:

$$H.R. = Q_{dry}/Q_{total}$$
 (28)

Increase of H.R. causes the water loss to be reduced but dictates use of more heat transfer area in the dry section.

Table 11 Parallel arrangement (winter).

Hybrid ratio	0.2	0.4	0.6	0.8	1
Wet cooling load (MW)		110.768	73.846	36.923	0
Total water loss (m3/h)	213.8	171	114.1	57	0
Required area (m ²)	22,510.4	45,022.1	67,539.9	89,996.8	112,556

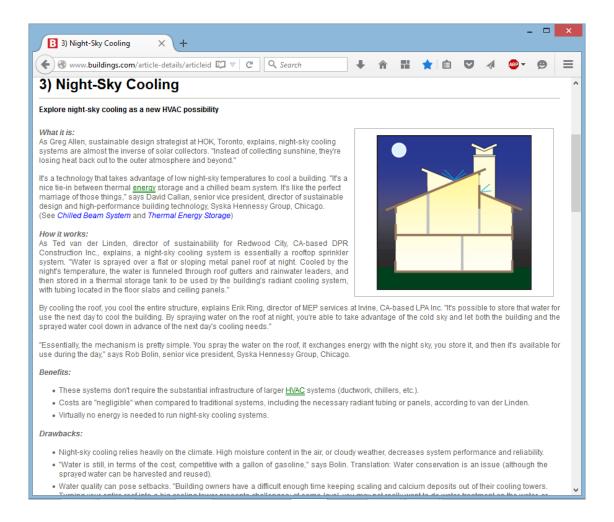
Table 12 Series arrangement (winter).

Hybrid ratio	0.2	0.4	0.6	0.8
Wet cooling load (MW)	147.691	110,768	73.846	36.923
Total water loss (m ³ /h)	220.8	176.5	124.5	77
Required area (m ²)	20,464.8	40,905.5	61,394.1	81,848.7

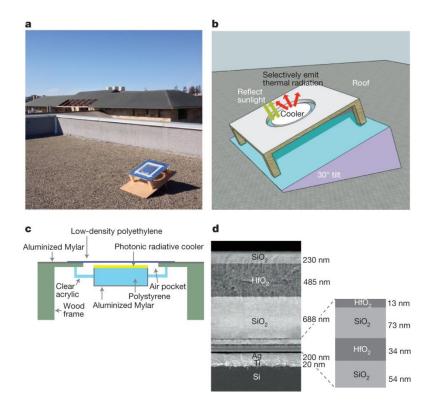
E. Rezaei, S. Shafiei and A. Abdollahnezhad, "Reducing water consumption of an industrial plant cooling unit using hybrid cooling tower," *Energy Conversion and Management*, vol. 51, pp. 311-319, 2010.

http://dx.doi.org/10.1016/j.enconman.2009.09.027.

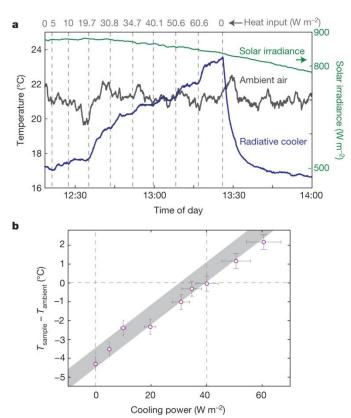
Skip this



Rooftop apparatus and photonic radiative cooler.



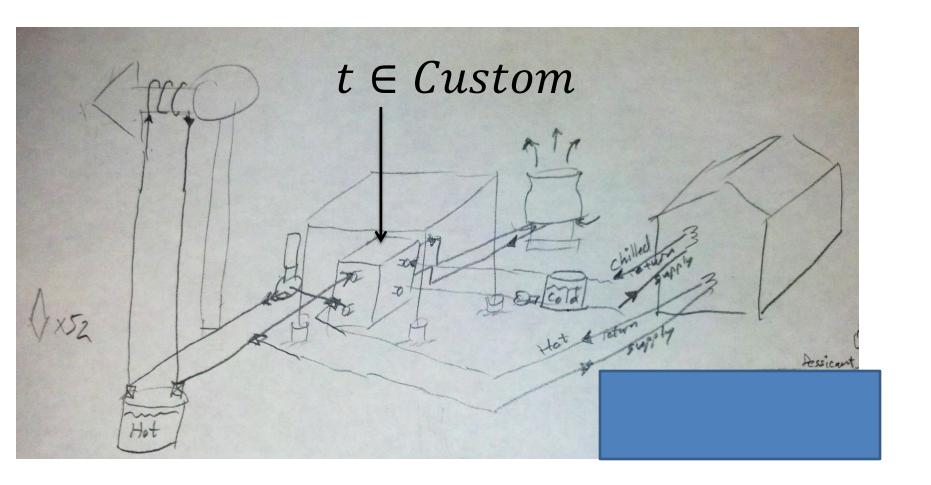
Cooling power of photonic radiative cooler.



AP Raman et al. Nature 515, 540-544 (2014) doi:10.1038/nature13883



Nick's dissertation Chapter 1



Multiple chillers

Assume: exergetic efficiency of chiller = 37 % (calculated based on Thermax LiBr single & double effect)

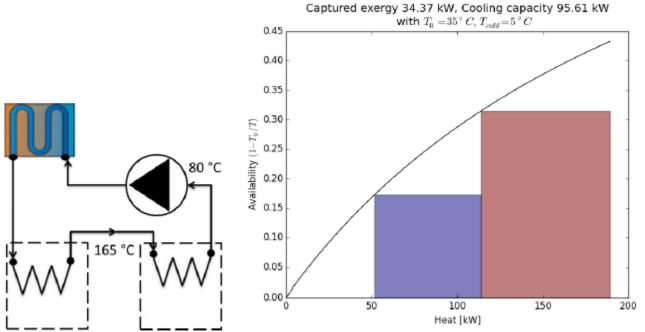


Figure 34. Multiple chillers drawing heat from heat source in series: conceptual schematic (left, not actual temperatures) and rescaled heat exchange diagram (right). Box areas show exergy supplied to the high effect chiller (red) and low effect (blue).

Multiple chillers: analytic result

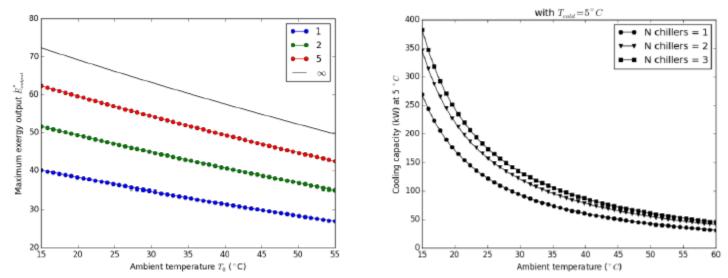


Figure 35. Multiple chillers: naïve model trends for optimal configurations.

High ambient temperature

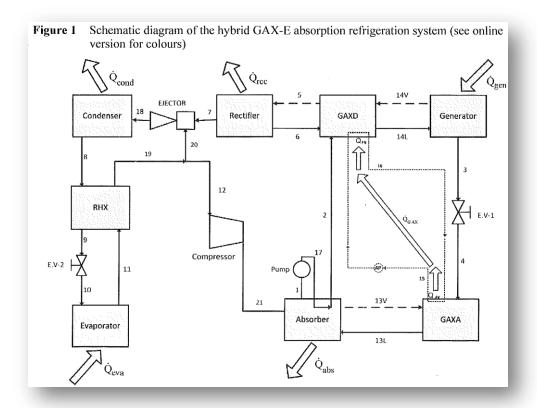


Figure 1. A cycle modified to recover energy from refrigerant expansion, from [40].

[40] A. Mehr, S. Mahmoudi, M. Yari and A. Soroureddin, "A novel hybrid GAX-ejector refrigeration cycle with an air-cooled absorber," *International Journal of Exergy*, vol. 13, no. 4, pp. 447-471, 2013.

Dynamic modelling users group?

- Modelica: a dynamic modelling language
- My application
 - Open source model (eventually dynamic) for absorption chiller
 - Requires: Open source library for properties (based on work from Spring, openACHP ...)
- Other applications
 - Building controls optimization

Solar tea?

